



## Vacuum Systems

Why much of physics sucks

# Why Vacuum?

- Anything cryogenic (or just very cold) needs to get rid of the air
  - eliminate thermal convection; avoid liquefying air
- Atomic physics experiments must get rid of confounding air particles
  - eliminate collisions
- Sensitive torsion balance experiments must not be subject to air
  - buffeting, viscous drag, etc. are problems
- Surface/materials physics must operate in pure environment
  - e.g., control deposition of atomic species one layer at a time

# Measures of pressure

- The “proper” unit of measure for pressure is Pascals (Pa), or  $\text{N}\cdot\text{m}^{-2}$
- Most vacuum systems use Torr instead
  - based on mm of Hg
- Atmospheric pressure is:
  - 760 Torr
  - 101325 Pa
  - 1013 mbar
  - 14.7 psi
- So 1 Torr is 133 Pa, 1.33 mbar; *roughly* one milli-atmosphere

# Properties of a vacuum

Vacuum	Pressure (torr)	Number Density ( $\text{m}^{-3}$ )	M.F.P. (m)	Surface Collision Freq. ( $\text{m}^{-2}\cdot\text{s}^{-1}$ )	Monolayer Formation Time (s)
Atmosphere	760	$2.7 \times 10^{25}$	$7 \times 10^{-8}$	$3 \times 10^{27}$	$3.3 \times 10^{-9}$
Rough	$10^{-3}$	$3.5 \times 10^{19}$	0.05	$4 \times 10^{21}$	$2.5 \times 10^{-3}$
High	$10^{-6}$	$3.5 \times 10^{16}$	50	$4 \times 10^{18}$	2.5
Very high	$10^{-9}$	$3.5 \times 10^{13}$	$50 \times 10^3$	$4 \times 10^{15}$	$2.5 \times 10^3$
Ultrahigh	$10^{-12}$	$3.5 \times 10^{10}$	$50 \times 10^6$	$4 \times 10^{12}$	$2.5 \times 10^6$



# Kinetic Theory

- The particles of gas are moving randomly, each with a unique velocity, but following the Maxwell Boltzmann distribution:

$$f(v) = \left( \frac{m}{2\pi kT} \right)^{\frac{3}{2}} e^{-mv^2/2kT}$$

- The average speed is:

$$\bar{v} = \left( \frac{8kT}{\pi m} \right)^{\frac{1}{2}}$$

- With the molecular weight of air around 29 g/mole (~75% N<sub>2</sub> @ 28; ~25% O<sub>2</sub> @ 32), 293 °K:
  - $m = 29 \times 1.67 \times 10^{-27}$  kg
  - $\langle v \rangle = 461$  m/s
  - note same ballpark as speed of sound (345 m/s)

# Mean Free Path

- The mean free path is the typical distance traveled before colliding with another air molecule
- Treat molecules as spheres with radius,  $r$
- If (the center of) another molecule comes within  $2r$  of the path of a select molecule:
- Each molecule sweeps out cylinder of volume:

$$V = 4\pi r^2 vt$$

- in time  $t$  at velocity  $v$

- If the volume density of air molecules is  $n$  (e.g.,  $\text{m}^{-3}$ ):
  - the number of collisions in time  $t$  is

$$nZ = 4\pi nr^2 vt$$

- Correcting for relative molecular speeds, and expressing as collisions per unit time, we have:

$$Z = 4\sqrt{2}\pi nr^2 v$$

## Mean Free Path, cont.

- Now that we have the collision frequency,  $Z$ , we can get the average distance between collisions as:

$$\lambda = v/Z$$

- So that

$$\lambda = \frac{1}{4\sqrt{2}\pi nr^2}$$

- For air molecules,  $r \approx 1.75 \times 10^{-10}$  m
- So  $\lambda \approx 6.8 \times 10^{-8}$  m = 68 nm at atmospheric pressure
- Note that mean free path is inversely proportional to the number density, which is itself proportional to pressure
- So we can make a rule for  $\lambda = (5 \text{ cm}) / (P \text{ in mtorr})$

# Relevance of Mean Free Path

- Mean free path is related to thermal conduction of air
  - if the mean free path is shorter than distance from hot to cold surface, there is a collisional (conductive) heat path between the two
- Once the mean free path is comparable to the size of the vessel, the paths are ballistic
  - collisions cease to be important
- Though not related in a 1:1 way, one also cares about transition from bulk behavior to molecular behavior
  - above 100 mTorr (about 0.00013 atm), air is still collisionally dominated (viscous)
    - $\lambda$  is about 0.5 mm at this point
  - below 100 mTorr, gas is molecular, and flow is statistical rather than viscous (bulk air no longer pushes on bulk air)

# Gas Flow Rates

- At some aperture (say pump port on vessel), the flow rate is

$$S = dV/dt \text{ (liters per second)}$$

- A pump is rated at a flow rate:

$$S_p = dV/dt \text{ at pump inlet}$$

- The mass rate through the aperture is just:

$$Q = PS \text{ (Torr liter per second)}$$

- And finally, the ability of a tube or network to conduct gas is

$$C \text{ (in liters per second)}$$

- such that

$$Q = (P_1 - P_2) \times C$$

# Evacuation Rate

- What you care about is evacuation rate of vessel

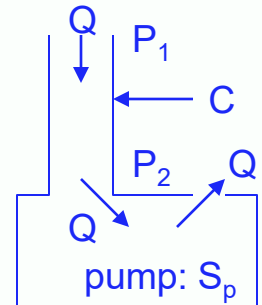
- $S = Q/P_1$

- but pump has  $S_p = Q/P_2$

- $Q$  is constant (conservation of mass)

- $Q = (P_1 - P_2)C$ , from which you can get:

$$1/S = 1/S_p + 1/C$$



- So the net flow looks like the “parallel” combination of the pump and the tube:

- the more restrictive will dominate

- Usually, the tube *is* the restriction

- example in book has 100 l/s pump connected to tube 2.5 cm in diameter, 10 cm long, resulting in flow of 16 l/s

- pump capacity diminished by factor of 6!

# Tube Conductance

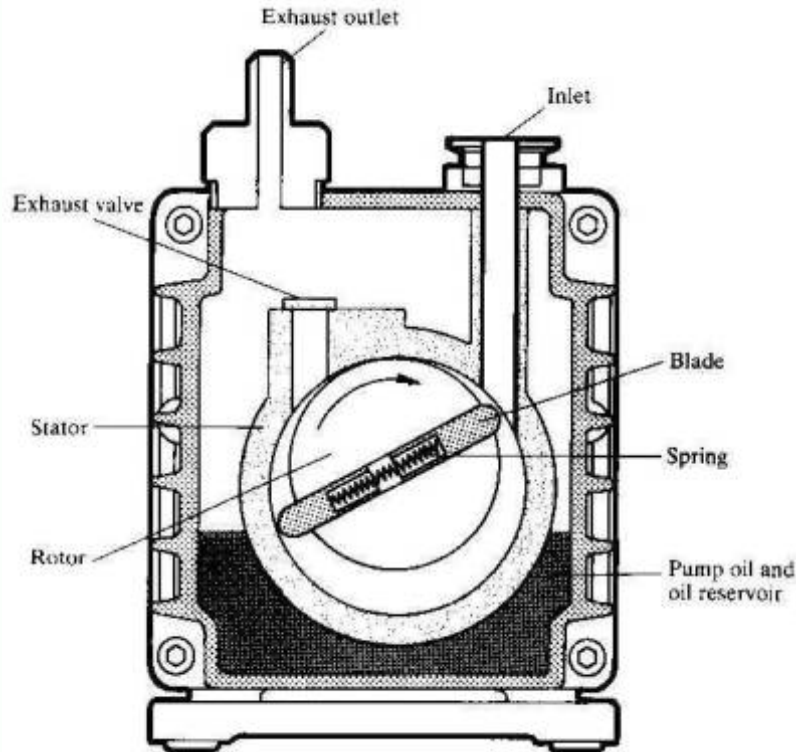
- For air at 293 K:
- In bulk behavior ( $> 100$  mTorr):
$$C = 180 \times P \times D^4 / L \quad (\text{liters per second})$$
  - $D$ , the diameter, and  $L$ , the length are in cm;  $P$  in Torr
  - note the *strong* dependence on diameter!
  - example: 1 m long tube 5 cm in diameter at 1 Torr:
    - allows 1125 liters per second
- In molecular behavior ( $< 100$  mTorr):
$$C = 12 \times D^3 / L$$
  - now cube of  $D$
  - same example, at 1 mTorr:
    - allows 0.1 liters per second (much reduced!)

# Pump-down time

- Longer than you wish
  - Viscous air removed quickly, then long slow process to remove rest
  - to go from pressure  $P_0$  to  $P$ , takes  $t = (V/S) \times \ln(P_0/P)$
  - note logarithmic performance



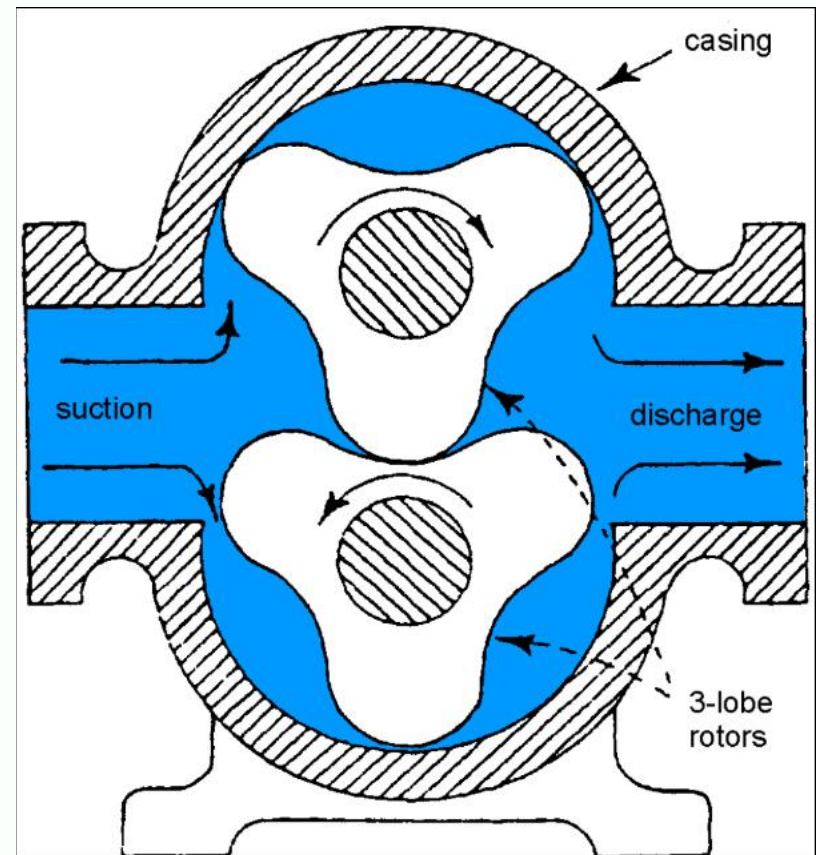
# Mechanical Pumps



- Form of “positive displacement pump”
- For “roughing,” or getting the the bulk of the air out, one uses mechanical pumps
  - usually rotary oil-sealed pumps
  - these give out at  $\sim 1\text{--}10$  mTorr
- A blade sweeps along the walls of a cylinder, pushing air from the inlet to the exhaust
- Oil forms the seal between blade and wall

# Lobe Injection Pumps

- Can move air very rapidly
- Often no oil seal
- Compression ratio not as good



# Turbomolecular pumps

- After roughing, one often goes to a turbo-pump
  - a fast (24,000 RPM) blade achieves a speed comparable to the molecular speed
  - molecules are mechanically deflected downward
- Work only in molecular regime
  - use after roughing pump is spent ( $< 100$  mTorr)
- Usually keep roughing pump on exhaust

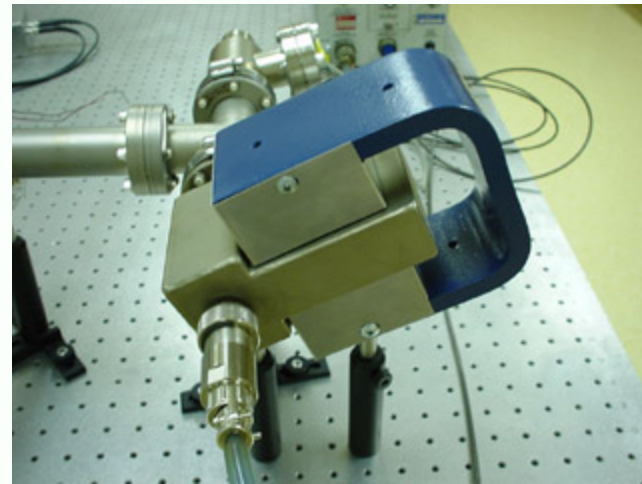
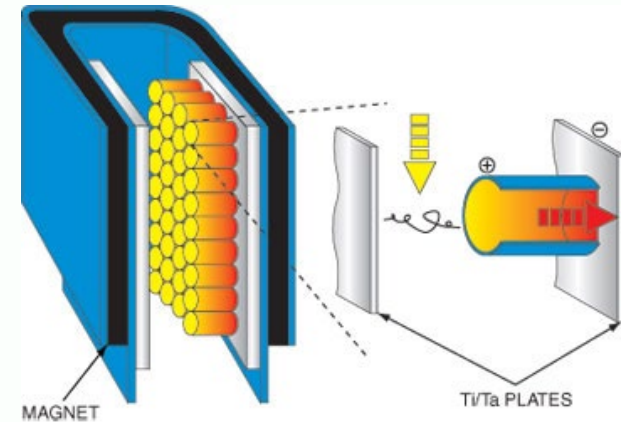


# Cryopumping

- A cold surface condenses volatiles (water, oil, etc.) and even air particles if sufficient nooks and crannies exist
  - a dessicant, or getter, traps particles of gas in cold molecular-sized “caves”
- Put the getter in the coldest spot
  - helps guarantee this is where particles trap: don’t want condensation on critical parts
  - when cryogen added, getter gets cold first
- Essentially “pumps” remaining gas, and even continued outgassing
- Called cryo-pumping

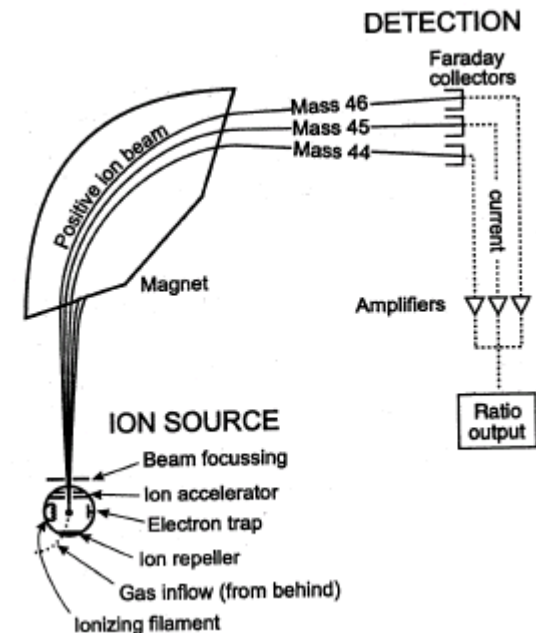
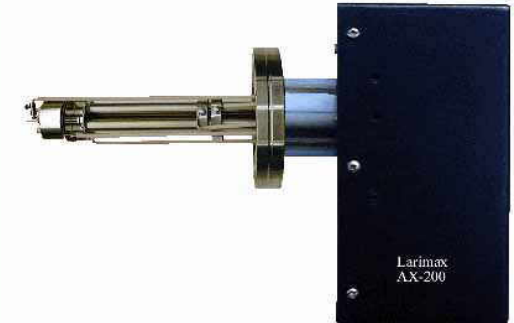
# Ion Pump

- Ionize gas molecules, deposit ions on chemically active surface, removed by chemisorption
- Best use is for Ultra-High Vacuum applications ( $10^{-11}$  Torr)
- Current is proportional to pressure (pump is also a pressure gauge)
- No moving parts, but efficient only at very low pressures



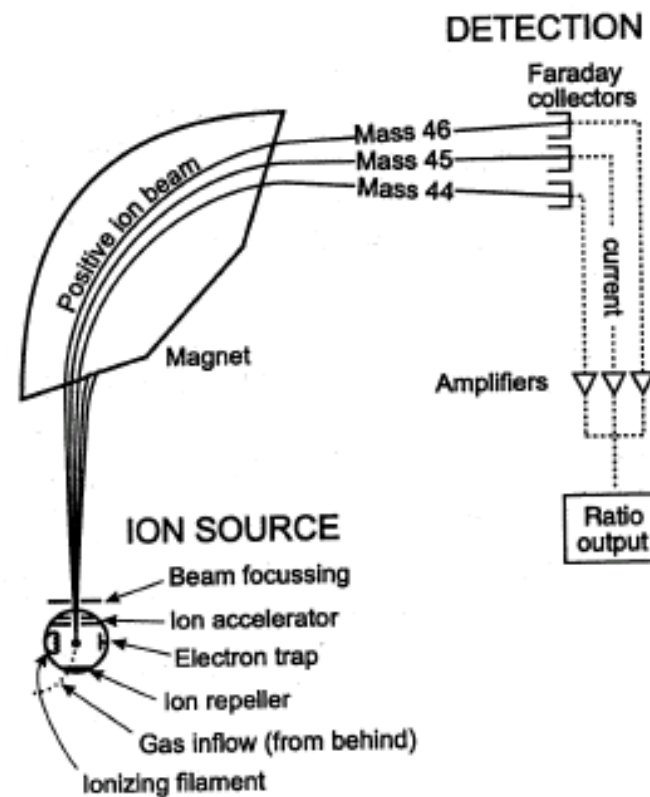
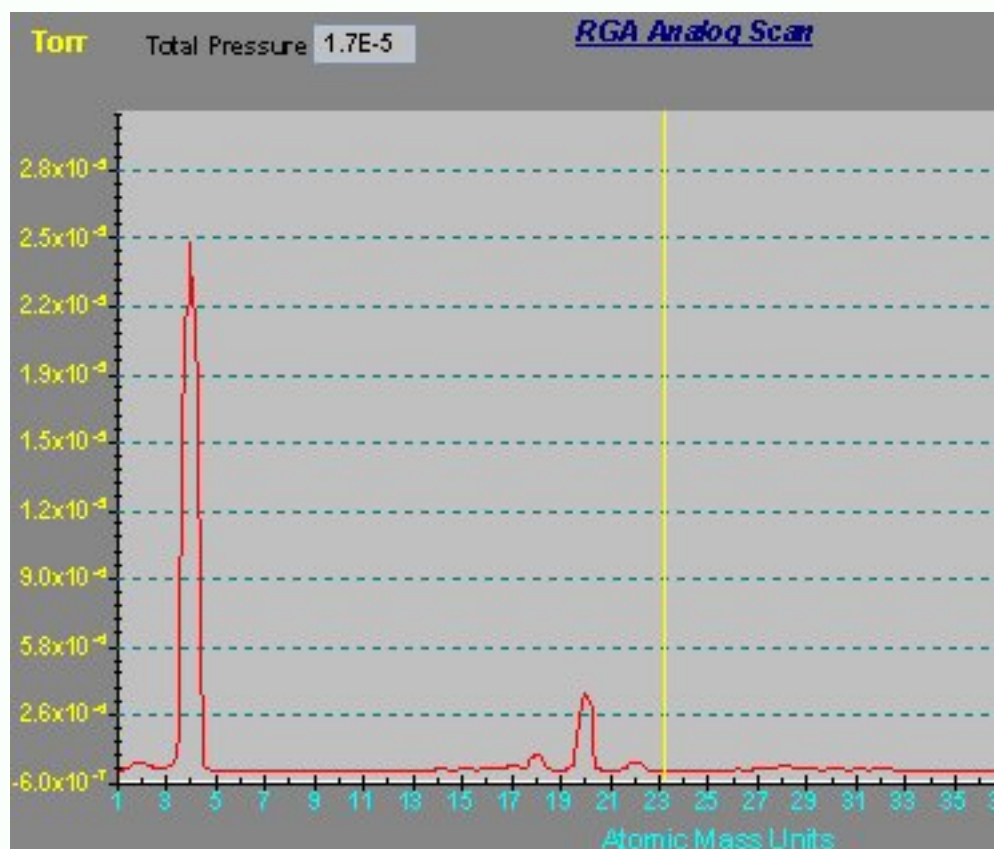
# Residual Gas Analyzer (mass spectrometer)

- Electronic “nose”, sniffing inside the chamber
- Can detect partial pressure down to  $10^{-14}$  Torr
- Useful as a He leak-detector
- Measures mass-to-charge ratio by ionizing a molecule and accelerating in EM field





# Example of RGA spectra, He:Ne mixture 10:1



# Typical problems in achieving UHV:

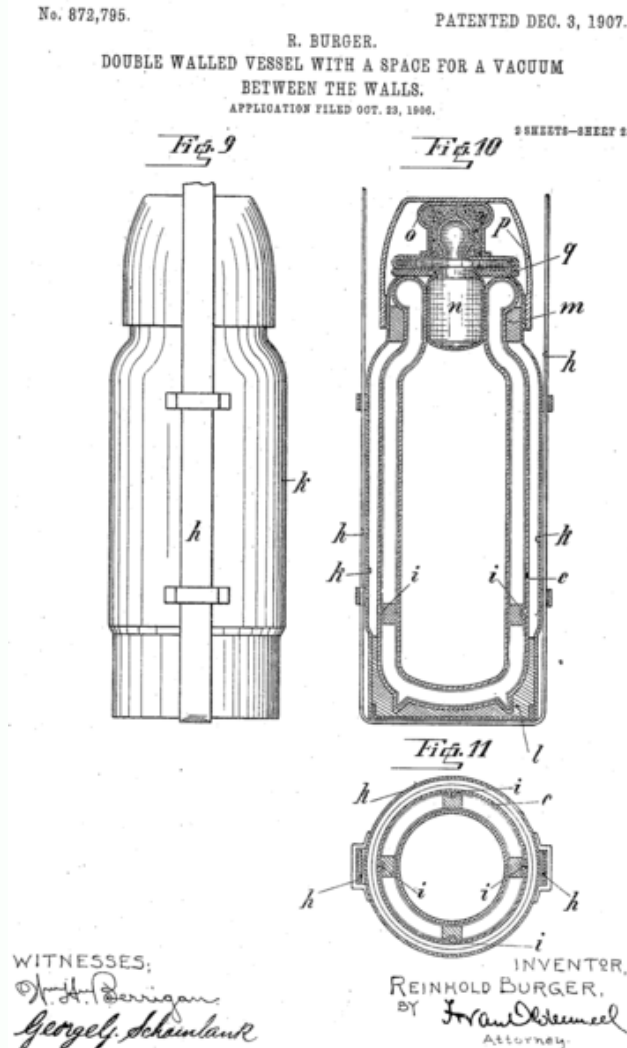
- Actual Leaks (valves, windows)
- Slow pump-down times
- “Virtual” leaks
- Outgassing – bulk and surfaces

## Solutions:

- Leak-testing
- Re-design of vacuum chamber
- Bake-out
- Cryopumping



# Dewars

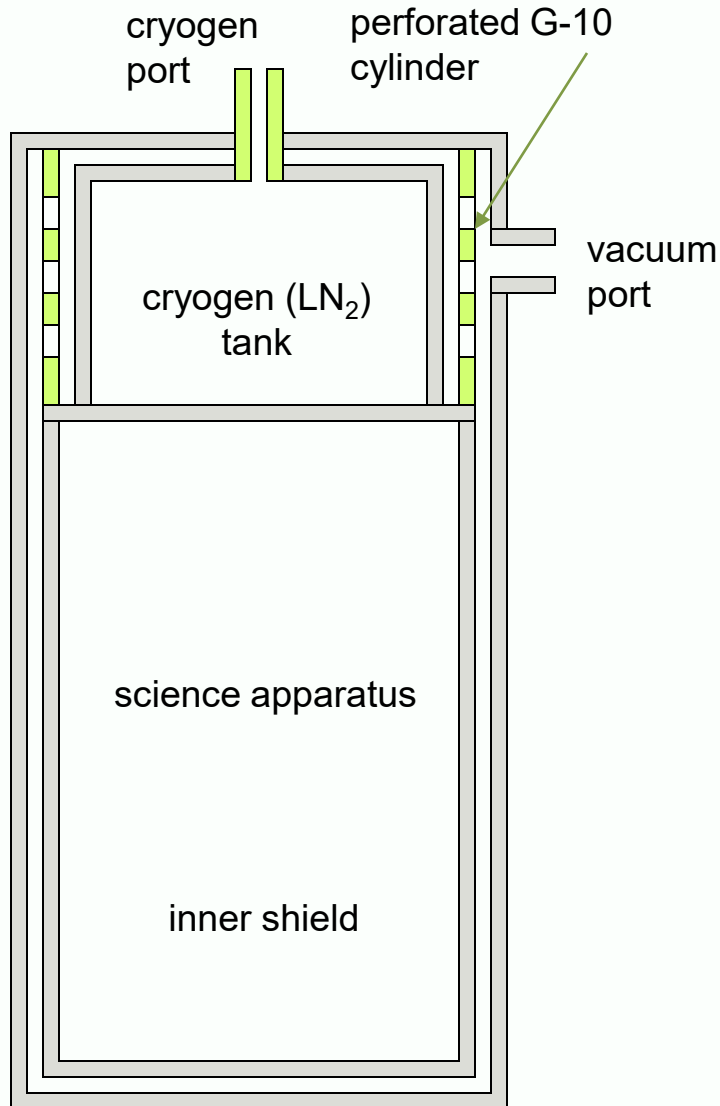


- Evacuating the region between the cold/hot wall and the ambient wall eliminates convection and direct air conduction
- Some conduction over the lip, through material
  - minimized by making thin and out of thermally non-conductive material
- Radiation is left, but suppressed by making all surfaces low emissivity (shiny)
- Heat paths cut → holds temperature of fluid

# Liquid Nitrogen Dewar

- Many Dewars are passively cooled via liquid nitrogen, at 77 K
- A bath of LN<sub>2</sub> is in good thermal contact with the “inner shield” of the dewar
- The connection to the outer shield, or pressure vessel, is thermally weak (though mechanically strong)
  - G-10 fiberglass is good for this purpose
- Ordinary radiative coupling of  $\sigma(T_h^4 - T_c^4) = 415 \text{ W/m}^2$  is cut to a few W/m<sup>2</sup>
  - Gold plating or aluminized mylar are often good choices
  - bare aluminum has  $\epsilon \approx 0.04$
  - gold is maybe  $\epsilon \approx 0.01$
  - aluminized mylar wrapped in many layered sheets is common (MLI: multi-layer insulation)
  - MLI wants to be punctured so-as not to make gas traps: makes for sloooooow pumping

# Dewar Construction



- Cryogen is isolated from warm metal via G-10
  - but in good thermal contact with inner shield
- Metal joints welded
- Inner shield gold-coated or wrapped in MLI to cut radiation
- Windows have holes cut into shields, with vacuum-tight clear window attached to outside
- Can put another, nested, inner-inner shield hosting liquid helium stage

pressure vessel/outer shield

# Cryogen Lifetime

- Note that  $\text{LN}_2$  in a bucket in a room doesn't go "poof" into gas
  - holds itself at 77 K: does not creep to 77.1K and all evaporate
  - due to finite "heat of vaporization"
    - $\text{LN}_2$  is 5.57 kJ/mole, 0.81 g/mL, 28 g/mol  $\rightarrow$  161 J/mL
    - $\text{L}^4\text{He}$  is 0.0829 kJ/mol, 0.125 g/mL, 4 g/mol  $\rightarrow$  2.6 J/mL
    - $\text{H}_2\text{O}$  is 40.65 kJ/mol, 1.0 g/mL, 18 g/mol  $\rightarrow$  2260 J/mL
- If you can cut the thermal load on the inner shield to 10 W, one liter of cryogen would last
  - 16,000 s  $\approx$  4.5 hours for  $\text{LN}_2$
  - 260 s  $\approx$  4 minutes for LHe

# Nested Shields

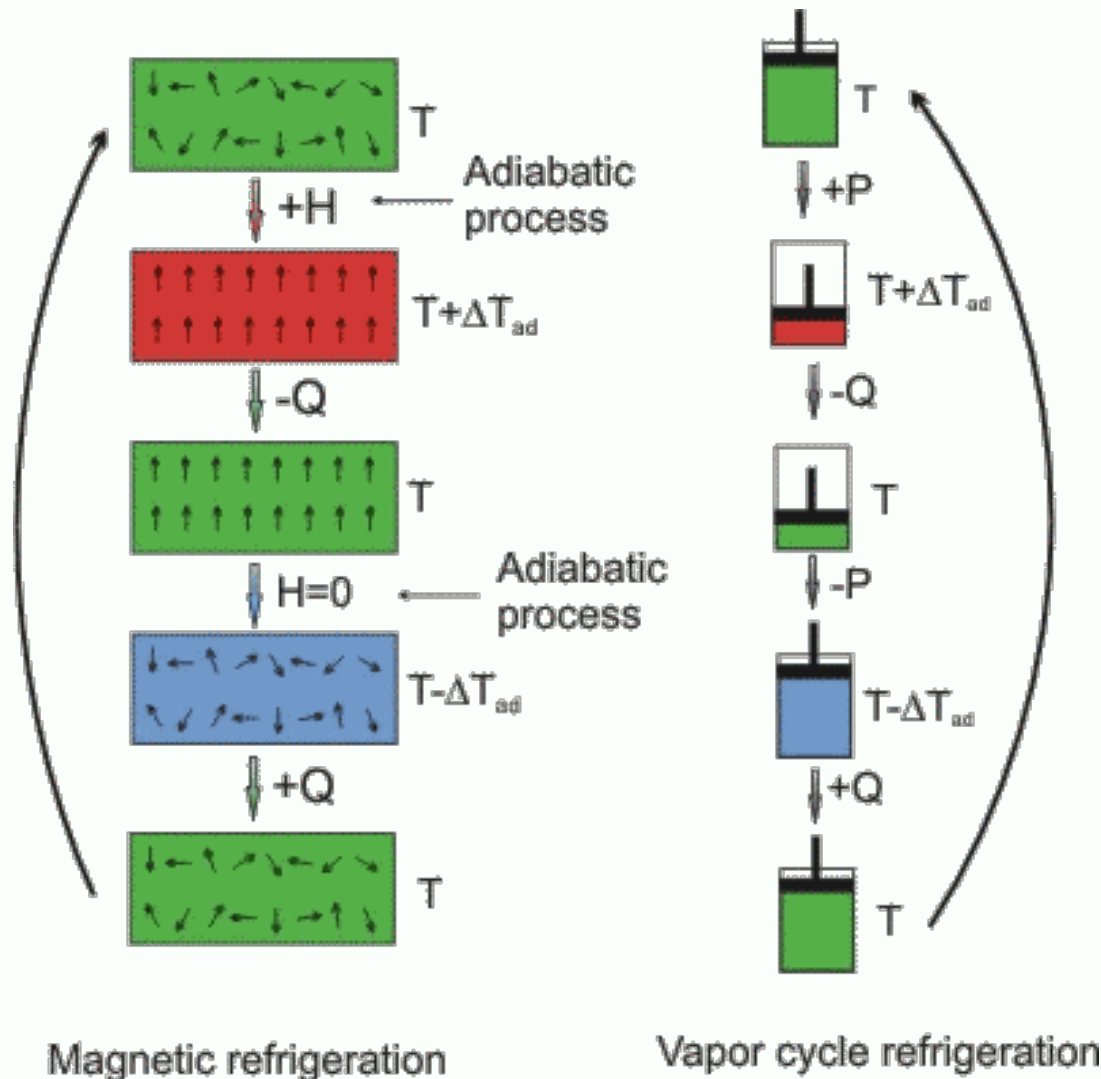
- LHe is expensive, thus the need for nested shielding
- Radiative load onto He stage much reduced if surrounded by 77 K instead of 293 K
  - $\sigma(293^4 - 4^4) = 418 \text{ W/m}^2$
  - $\sigma(77^4 - 4^4) = 2.0 \text{ W/m}^2$
  - so over 200 times less load for same emissivity
  - instead of a liter lasting 4 minutes, now it's 15 hours!
  - based on 10 W load for same configuration at LN<sub>2</sub>

# Coollest place on earth:

- Antarctica  $-89^{\circ}$  C, or 183K
- San Diego: Dilution fridges  
Mayer Hall (Maple, Goodkind), NSB (Butov)  $\sim 300$  mK
- Cambridge, MA: Sub-500 picoKelvin achieved in Ketterle group at MIT

See “**Cooling Bose-Einstein Condensates Below 500 Picokelvin**”  
*Science* 301, 5639 pp. 1513 - 1515 (2003)

# Adiabatic Magnetization Cooling



Magnetic refrigeration

Vapor cycle refrigeration

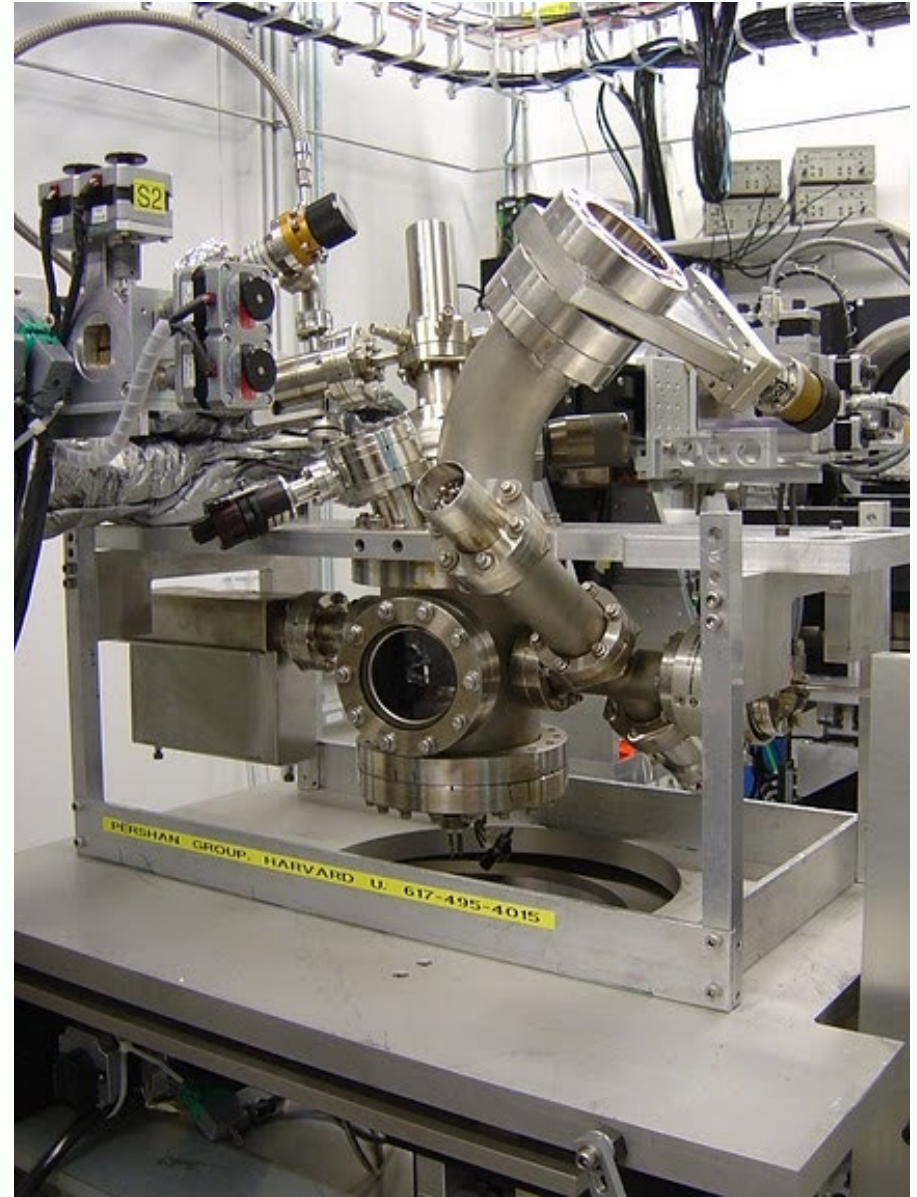


# Photos: Displex Cryostat insert



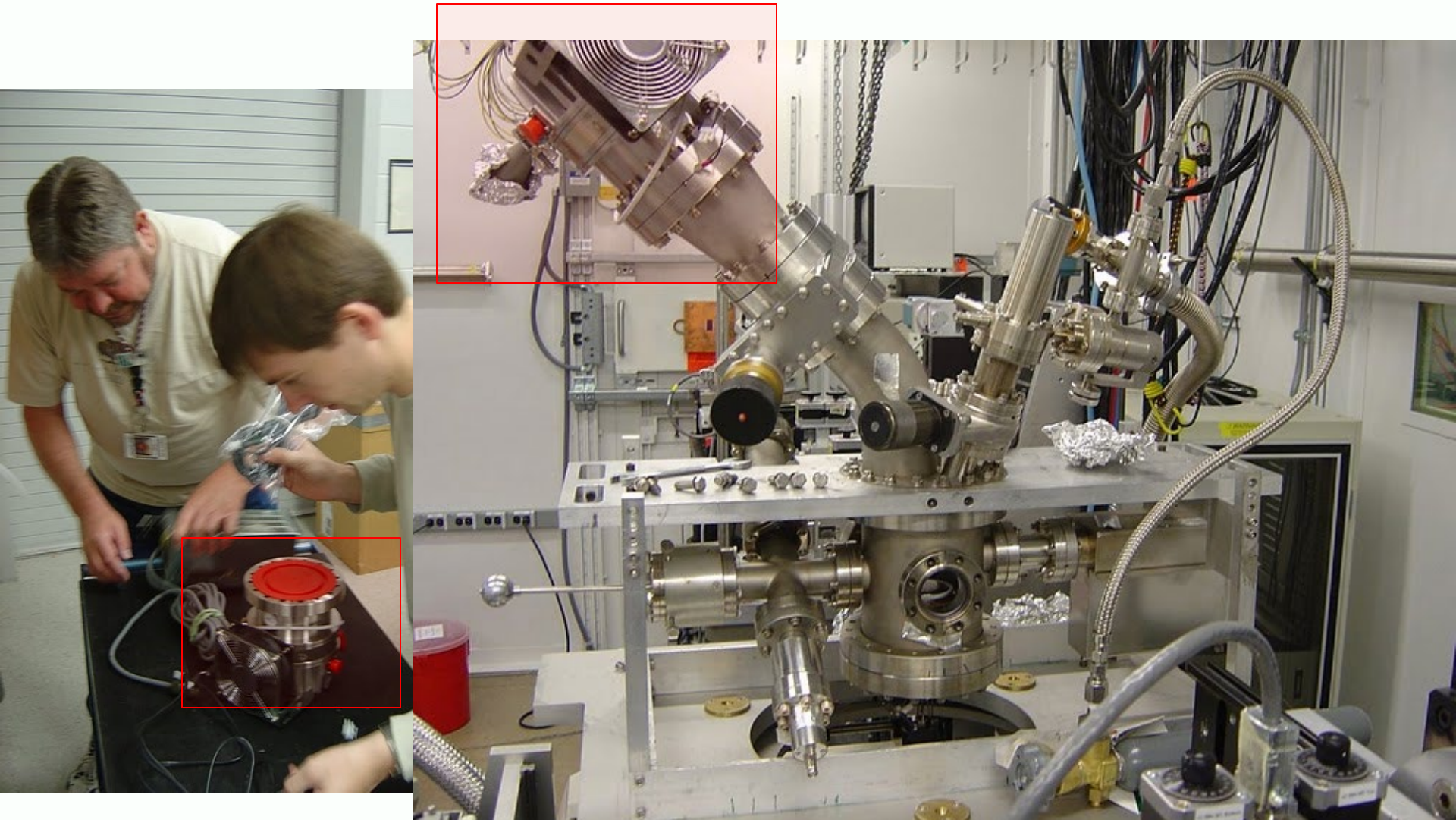


# Photos: Ultra High Vacuum chamber



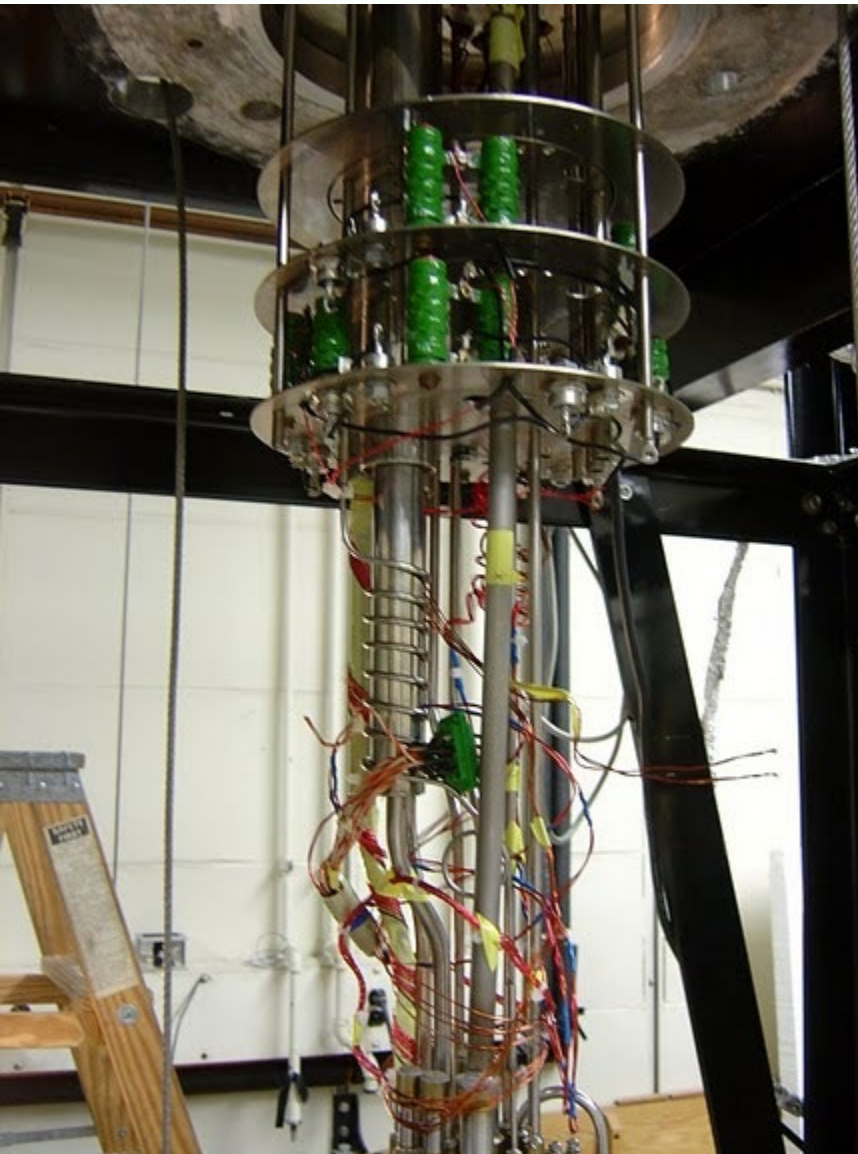


# Photos: Turbomolecular “Turbo” Pump



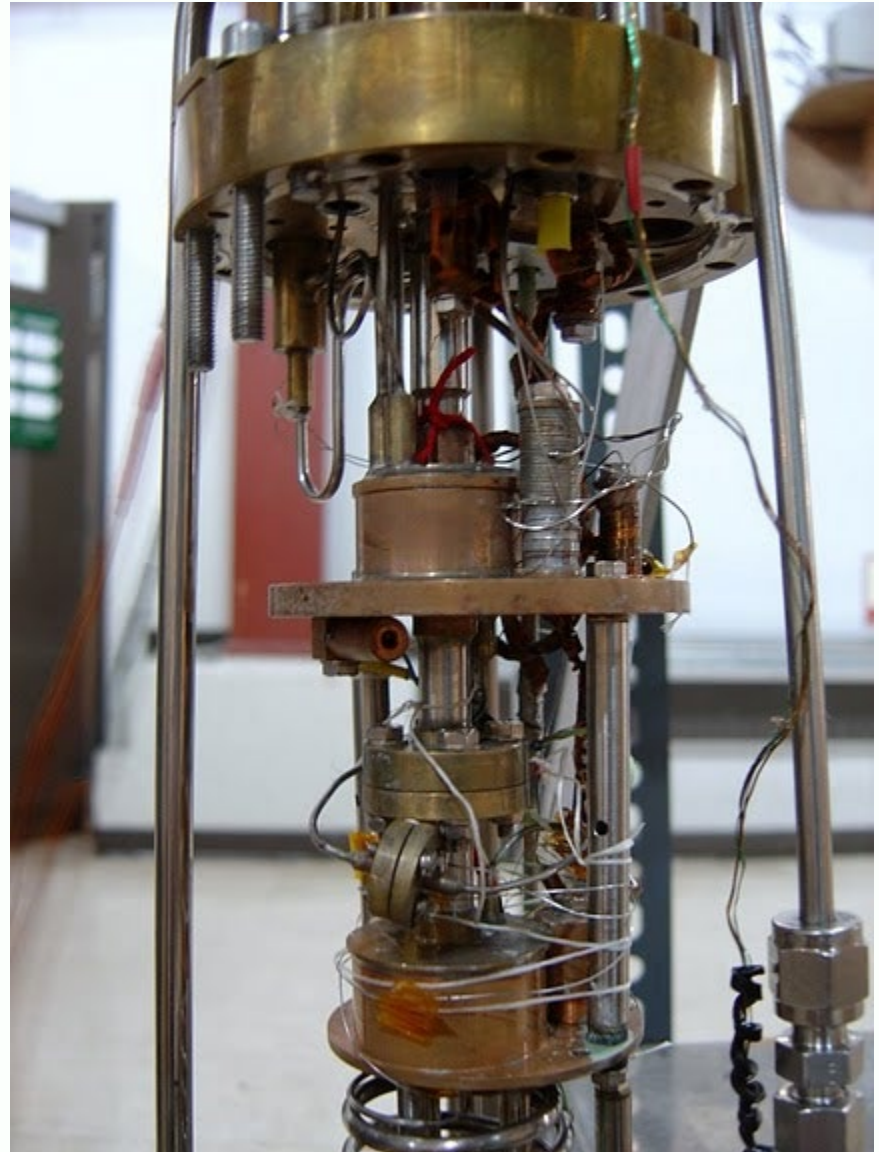
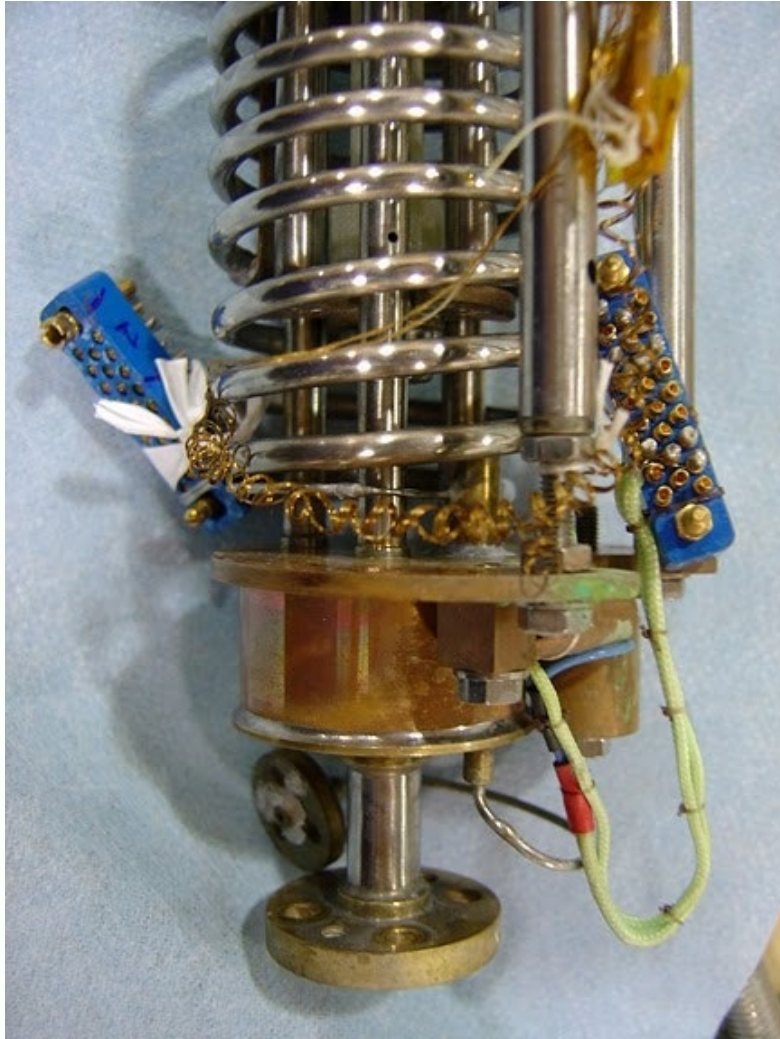


# Photos: Dilution Refrigerator

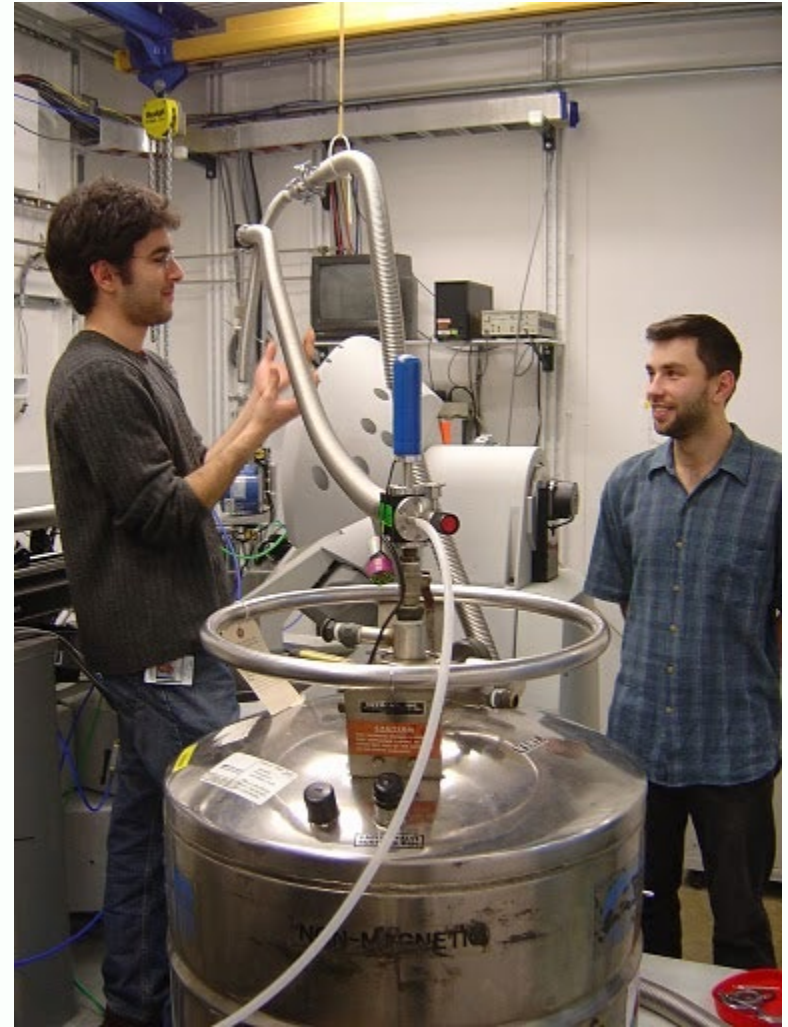
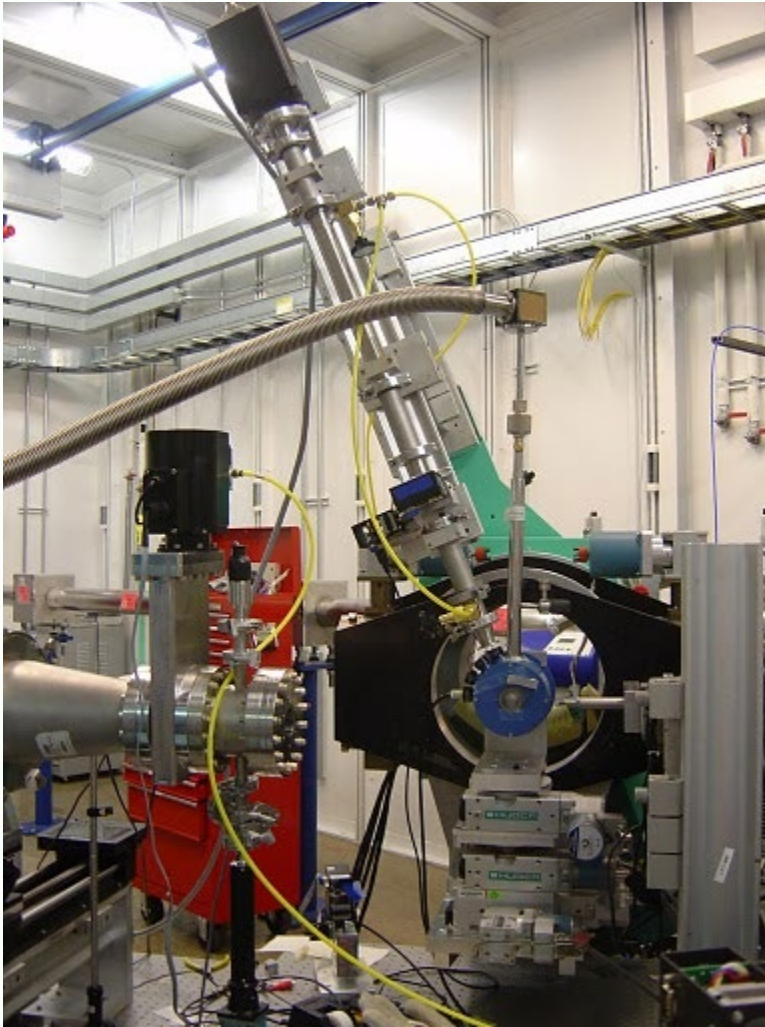




# Photos: Dilution Refrigerator



# Helium Flow Cryostat



# Assignments

- Read 3.1, 3.2, 3.3.2, 3.3.4, 3.4: 3.4.1 (Oil-sealed and Turbomolecular, 3.4.3 (Getter and Cryo), 3.5.2 (O-ring joints), 3.6.3, 3.6.5
  - applies to both 3<sup>rd</sup> and 4<sup>th</sup> editions